

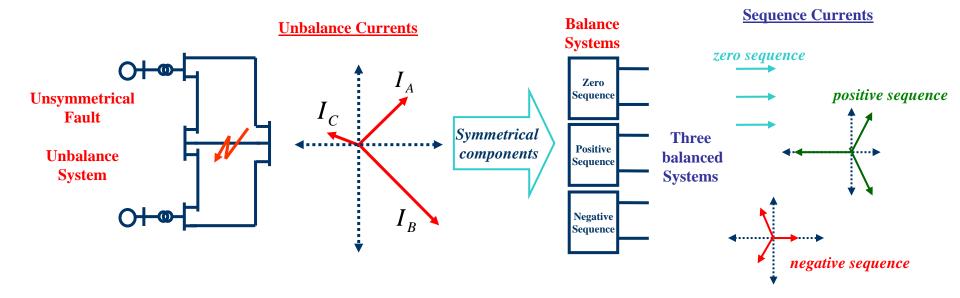
ELE B7 Power Systems Engineering

Symmetrical Components

Analysis of Unbalanced Systems

- Except for the balanced three-phase fault, faults result in an unbalanced system.
- The most common types of faults are single lineground (SLG) and line-line (LL). Other types are double line-ground (DLG), open conductor, and balanced three phase.
- The easiest method to analyze unbalanced system operation due to faults is through the use of symmetrical components

- The key idea of symmetrical component analysis is to decompose the unbalanced system into three sequence of balanced networks. The networks are then coupled only at the point of the unbalance (i.e., the fault)
- The three sequence networks are known as the
 - positive sequence (this is the one we've been using)
 - negative sequence
 - zero sequence



Assuming three unbalance voltage phasors, V_A , V_B and V_C having a positive sequence (*abc*). Using symmetrical components it is possible to represent each phasor voltage as:

$$V_{A} = V_{A}^{0} + V_{A}^{+} + V_{A}^{-}$$

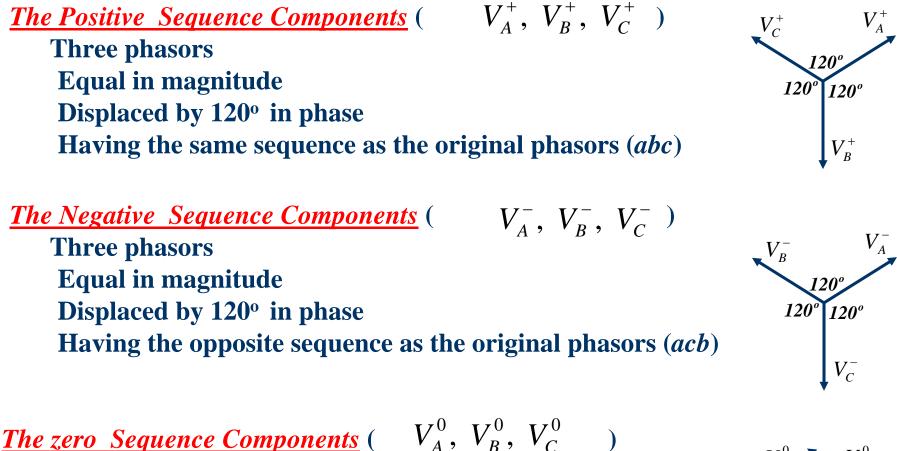
$$V_{B} = V_{B}^{0} + V_{B}^{+} + V_{B}^{-}$$

$$V_{C} = V_{C}^{0} + V_{C}^{+} + V_{C}^{-}$$

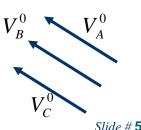
$$Negative Sequence Component$$

$$Negative Sequence Component$$

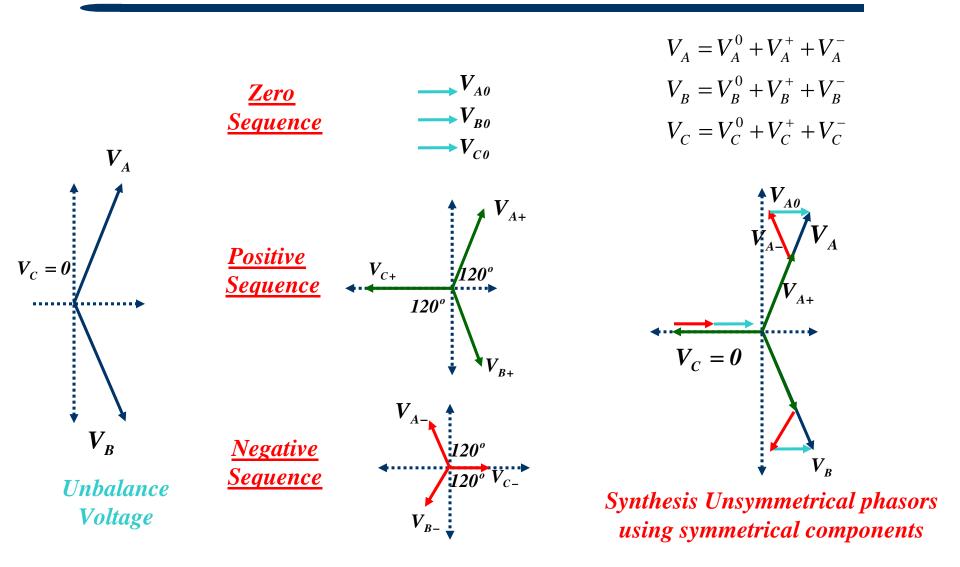
Where the symmetrical components are:



Three phasors Equal in magnitude Having the same phase shift (in phase)







Sequence Set Representation

• Any arbitrary set of three phasors, say I_a, I_b, I_c can be represented as a sum of the three sequence sets

$$I_{a} = I_{a}^{0} + I_{a}^{+} + I_{a}^{-}$$
$$I_{b} = I_{b}^{0} + I_{b}^{+} + I_{b}^{-}$$
$$I_{c} = I_{c}^{0} + I_{c}^{+} + I_{c}^{-}$$

where

 I_a^0, I_b^0, I_c^0 is the zero sequence set I_a^+, I_b^+, I_c^+ is the positive sequence set I_a^-, I_b^-, I_c^- is the negative sequence set

Conversion Sequence to Phase

Only three of the sequence values are unique, I_a^0, I_a^+, I_a^- ; the others are determined as follows: $\alpha = 1 \angle 120^{\circ}$ $\alpha + \alpha^2 + \alpha^3 = 0$ $\alpha^3 = 1$ $I_a^0 = I_b^0 = I_c^0$ (since by definition they are all equal) $I_{h}^{+} = \alpha^{2} I_{a}^{+}$ $I_{c}^{+} = \alpha I_{a}^{+}$ $I_{h}^{-} = \alpha I_{a}^{-}$ $I_{c}^{+} = \alpha^{2} I_{a}^{-}$ $\begin{bmatrix} I_a \\ I_b \\ I_c \end{bmatrix} = \mathbf{I}_a^0 \begin{bmatrix} 1 \\ 1 \\ 1 \end{bmatrix} + \mathbf{I}_a^+ \begin{bmatrix} 1 \\ \alpha^2 \\ \alpha \end{bmatrix} + I_a^- \begin{bmatrix} 1 \\ \alpha \\ \alpha^2 \end{bmatrix} = \begin{bmatrix} 1 & 1 & 1 \\ 1 & \alpha^2 & \alpha \\ 1 & \alpha & \alpha^2 \end{bmatrix} \begin{bmatrix} I_a \\ I_a \\ I_a \end{bmatrix}$

Conversion Sequence to Phase

Define the symmetrical components transformation matrix

$$\mathbf{A} = \begin{bmatrix} 1 & 1 & 1 \\ 1 & \alpha^2 & \alpha \\ 1 & \alpha & \alpha^2 \end{bmatrix}$$

Then
$$\mathbf{I} = \begin{bmatrix} I_a \\ I_b \\ I_c \end{bmatrix} = \mathbf{A} \begin{bmatrix} I_a^0 \\ I_a^+ \\ I_a^- \end{bmatrix} = \mathbf{A} \begin{bmatrix} I^0 \\ I^+ \\ I^- \end{bmatrix} = \mathbf{A} \mathbf{I}_s$$

Conversion Phase to Sequence

By taking the inverse we can convert from the phase values to the sequence values

$$\mathbf{I}_{s} = \mathbf{A}^{-1}\mathbf{I}$$

with $\mathbf{A}^{-1} = \frac{1}{3} \begin{bmatrix} 1 & 1 & 1 \\ 1 & \alpha & \alpha^{2} \\ 1 & \alpha^{2} & \alpha \end{bmatrix}$

Sequence sets can be used with voltages as well as with currents

Example

If the values of the fault currents in a three phase system are:

$$I_A = 150 \angle 45$$
 $I_B = 250 \angle 150$ $I_C = 100 \angle 300$

Find the symmetrical components?

Solution:

$$V_{+} = \frac{1}{3} \left(V_{A} + \alpha V_{B} + \alpha^{2} V_{C} \right)$$

$$V_{-} = \frac{1}{3} \left(V_{A} + \alpha^{2} V_{B} + \alpha V_{C} \right)$$

$$\frac{V_O}{O} = \frac{1}{3} \left(V_A + V_B + V_C \right)$$

$$I_{+} = \frac{1}{3} \left(I_{A} + \alpha I_{B} + \alpha^{2} I_{C} \right) = \frac{1}{3} \left(150 \angle 45^{\circ} + 250 \angle 270^{\circ} + 100 \angle 180^{\circ} \right)$$
$$= 48.02 \angle -87.6^{\circ}$$

$$I_{-} = \frac{1}{3} \left(I_{\mathcal{A}} + \alpha^2 I_{\mathcal{B}} + \alpha I_{\mathcal{C}} \right)$$

=163.21∠40.45

$$I_0 = \frac{1}{3} \left(I_A + I_B + I_C \right)$$

 $=\frac{1}{2}(106.04 + j106.07 + j106.07 - 216.51 + j125.00 + 50 - j86.6)$

= 52.2∠112.7

Example

If the values of the sequence voltages in a three phase system are:

 $V_0 = 100$ $V_+ = 200 \angle 60$ $V_- = 100 \angle 120$

Find the three phase voltages

Solution:

- $V_A = 200 \angle 60 + 100 \angle 120 + 100$ $V_A = 300 \angle 60$
- $V_B = 1 \angle 240(\ 200 \angle 60\) + 1 \angle 120(\ 100 \angle 120\) + 100$

 $V_B = 300 \angle -60$

 $V_C = 0$

 $V_C = 1 \angle 120(\ 200 \angle 60\) + 1 \angle 240(\ 100 \angle 120\) + 100$

 $V_{A} = V_{+} + V_{-} + V_{0}$

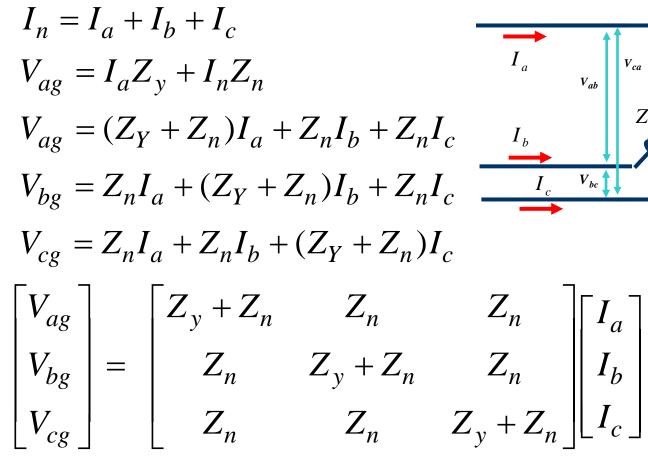
 $V_R = \alpha^2 V_+ + \alpha V_- + V_0$

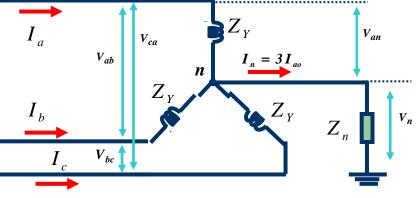
 $V_C = \alpha V_+ + \alpha^2 V_- + V_0$

Use of Symmetrical Components

1. The Sequence circuits for Wye and Delta connected loads

Consider the following Y-connected load:





Use of Symmetrical Components

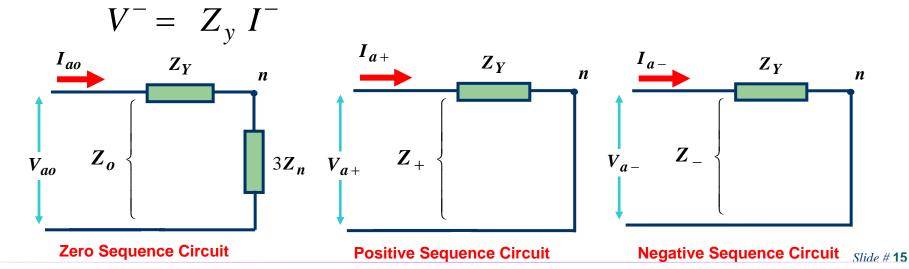
 $\begin{bmatrix} V_{ag} \\ V_{bg} \\ V_{cg} \end{bmatrix} = \begin{bmatrix} Z_y + Z_n & Z_n & Z_n \\ Z_n & Z_y + Z_n & Z_n \\ Z_n & Z_n & Z_y + Z_n \end{bmatrix} \begin{bmatrix} I_a \\ I_b \\ I_c \end{bmatrix}$ $\mathbf{V} = \mathbf{Z} \mathbf{I}, \quad \mathbf{V} = \mathbf{A} \mathbf{V}_s, \quad \mathbf{I} = \mathbf{A} \mathbf{I}_s$ $\mathbf{A} \mathbf{V}_s = \mathbf{Z} \mathbf{A} \mathbf{I}_s \longrightarrow \mathbf{V}_s = \mathbf{A}^{-1} \mathbf{Z} \mathbf{A} \mathbf{I}_s$ $\mathbf{A}^{-1} \mathbf{Z} \mathbf{A} = \begin{bmatrix} Z_y + 3Z_n & 0 & 0 \\ 0 & Z_y & 0 \\ 0 & 0 & Z_y \end{bmatrix}$

Networks are Now Decoupled

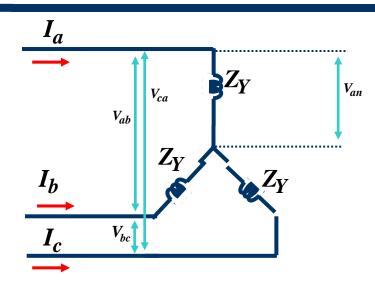
$$\begin{bmatrix} V^{0} \\ V^{+} \\ V^{-} \end{bmatrix} = \begin{bmatrix} Z_{y} + 3Z_{n} & 0 & 0 \\ 0 & Z_{y} & 0 \\ 0 & 0 & Z_{y} \end{bmatrix} \begin{bmatrix} I^{0} \\ I^{+} \\ I^{-} \end{bmatrix}$$

Systems are decoupled

 $V^{0} = (Z_{y} + 3Z_{n}) I^{0} \qquad V^{+} = Z_{y} I^{+}$



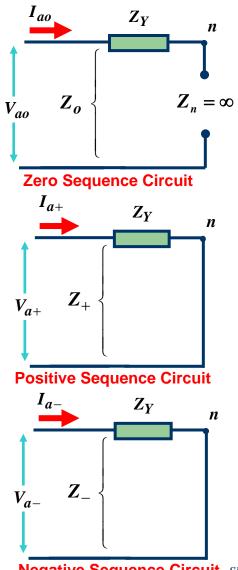
Y-connected load (Isolated Neutral):



If the neutral point of a Y-connected load is not grounded, therefore, no zero sequence current can flow, and

$$Z_n = \infty$$

Symmetrical circuits for Y-connected load with neutral point is not connected to ground are presented as shown:



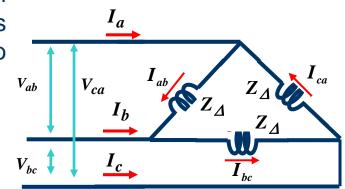
Negative Sequence Circuit *Slide* # 16

Delta connected load:

The Delta circuit can not provide a path through neutral. Therefore for a *Delta connected load* or its *equivalent Y-connected* can not contain any zero sequence components.

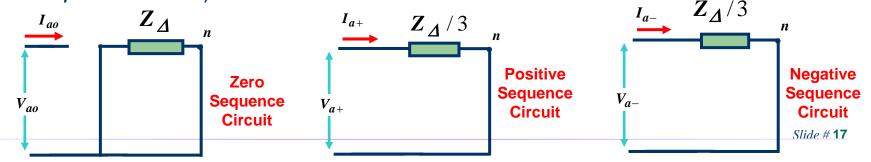
$$V_{ab} = Z_{\Delta}I_{ab}$$
, $V_{bc} = Z_{\Delta}I_{bc}$, $V_{ca} = Z_{\Delta}I_{ca}$

The summation of the line-to-line voltages or phase currents are always zero



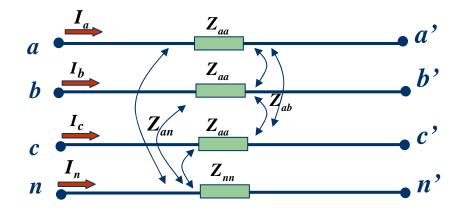
$$\frac{1}{3}(V_{ab} + V_{bc} + V_{ca}) = V_{ab0} = 0 \quad \text{and} \quad \frac{1}{3}(I_{ab} + I_{bc} + I_{ca}) = I_{ab0} = 0$$

Therefore, for a <u>**Delta-connected loads</u>** without sources or mutual coupling there will be no zero sequence currents at the lines (There are some cases where a circulating currents may circulate inside a delta load and not seen at the terminals of the zero sequence circuit).</u>



Sequence diagrams for lines

- Similar to what we did for loads, we can develop sequence models for other power system devices, such as lines, transformers and generators
- For transmission lines, assume we have the following, with mutual impedances



Sequence diagrams for lines, cont'd

Assume the phase relationships are

$\left\lceil \Delta V_a \right\rceil$		$\Box Z_s$	Z_m	Z_m	$\begin{bmatrix} I_a \end{bmatrix}$
ΔV_b	=	Z_m	Z_s	Z_m	I _b
ΔV_c		$\lfloor Z_m$	Z_m	$\begin{bmatrix} Z_m \\ Z_m \\ Z_s \end{bmatrix}$	$[I_c]$

where

 Z_s = self impedance of the phase

 Z_m = mutual impedance between the phases Writing in matrix form we have

 $\Delta \mathbf{V} = \mathbf{Z}\mathbf{I}$

Sequence diagrams for lines, cont'd

Similar to what we did for the loads, we can convert these relationships to a sequence representation $\Delta \mathbf{V} = \mathbf{Z} \mathbf{I} \quad \Delta \mathbf{V} = \mathbf{A} \Delta \mathbf{V}_s \qquad \mathbf{I} = \mathbf{A} \mathbf{I}_s$ $\mathbf{A} \Delta \mathbf{V}_s = \mathbf{Z} \mathbf{A} \mathbf{I}_s \rightarrow \Delta \mathbf{V}_s = \mathbf{A}^{-1} \mathbf{Z} \mathbf{A} \mathbf{I}_s$ $\mathbf{A}^{-1} \mathbf{Z} \mathbf{A} = \begin{bmatrix} Z_s + 2Z_m & 0 & 0 \\ 0 & Z_s - Z_m & 0 \\ 0 & 0 & Z_s - Z_m \end{bmatrix}$

Sequence diagrams for lines, cont'd

Therefore,

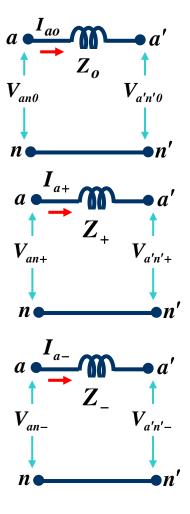
 $Z_o = Z_s + 2Z_m$ $Z_+ = Z_s - Z_m$ $Z_- = Z_s - Z_m$

<u>Where,</u>

 $Z_s = Z_{aa} + Z_{nn} - 2Z_{an}$

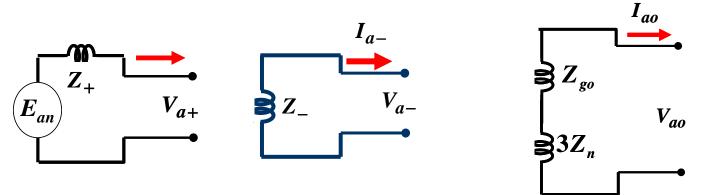
$$Z_m = Z_{ab} + Z_{nn} - 2Z_{an}$$

The ground wires (*above overhead TL*) combined with the earth works as a neutral conductor with impedance parameters that effects the zero sequence components. Having a good grounding (depends on the soil resistively), then the voltages to the neutral can be considered as the voltages to ground.



Sequence diagrams for generators

• Key point: generators only produce positive sequence voltages; therefore only the positive sequence has a voltage source



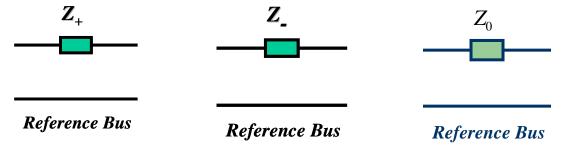
During a fault $Z^+ \approx Z^- \approx X_d^{"}$. The zero sequence impedance is usually substantially smaller. The value of Z_n depends on whether the generator is grounded

Sequence diagrams for Transformers

• The positive and negative sequence diagrams for transformers are similar to those for transmission lines.



 The zero sequence network depends upon both how the transformer is grounded and its type of connection. The easiest to understand is a double grounded wyewye



Transformer Sequence Diagrams

